# EE 330 Lecture 30

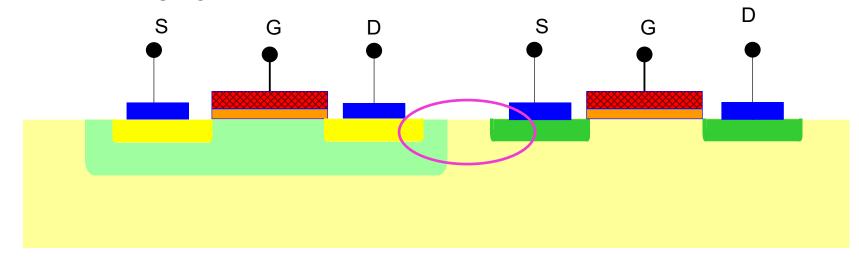
## **Thyristors**

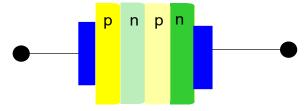
- SCR Basic circuits and limitations
- Triacs
- Other thyristor types

## The Thyristor

A bipolar device in CMOS Processes

#### Consider a Bulk-CMOS Process





Have formed a lateral pnpn device!

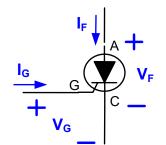
Will spend some time studying pnpn devices

# Operation of the SCR G $I_{\mathsf{F}}$ $Q_2$

Not actually separated but useful for describing operation

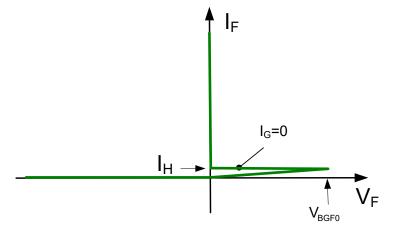
# Review from Last Lecture Operation of the SCR

Consider the Ideal SCR Model

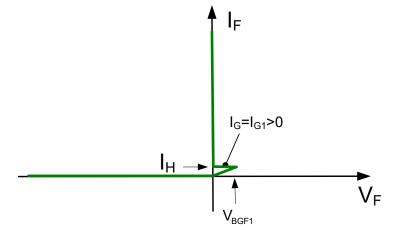


$$I_{F} = f_{1I}(V_{F}, I_{G})$$

$$I_{G} = f_{2I}(V_{G})$$



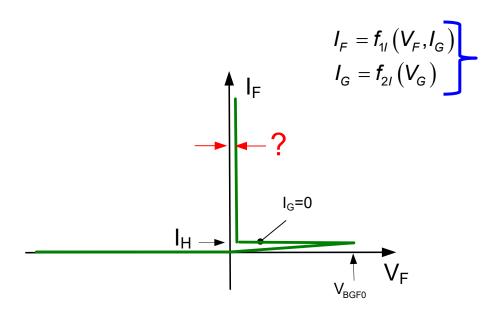
I<sub>H</sub> is very small

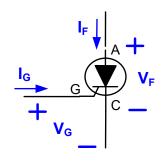


I<sub>G1</sub> is small (but not too small)

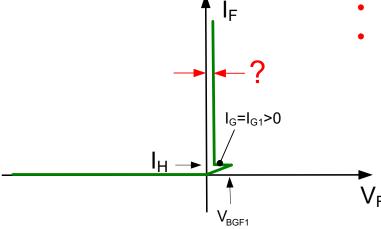
# Review from Last Lecture Operation of the SCR

Consider nearly Ideal SCR Model





- On voltage approximately 0.9V
  - Major contributor to ON-state power dissipation
- Even with large currents, P<sub>ON</sub> is quite small

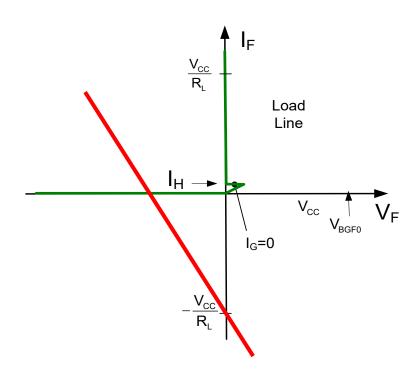


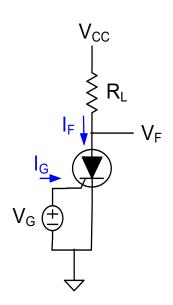
## Operation of the SCR

#### Operation with the Ideal SCR

Often V<sub>CC</sub> is an AC signal (often 110V)

SCR will turn off whenever AC signal goes negative





#### **Performance Limitations with the SCR**

 $V_{CC}$  $R_L$ Assume  $V_{CC}$  is an AC signal (often 110V) and  $V_{G}$  is static  $\frac{V_{\text{CC}}}{R_{\text{L}}}$ Load Line  $V_{cc}$  $V_{\mathsf{RL}}$ 

SCR is ON less than 50% of the time (duty cycle depends upon  $V_{\rm G}$ ) Often use electronic circuit to generate  $V_{\rm G}$ 

## **Outline**

## Two-Port Amplifier Models

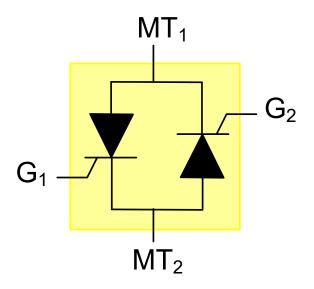
## **Bipolar Processes**

- Comparison of MOS and Bipolar Process
- Parasitic Devices in CMOS Processes
- JFET

## Special Bipolar Processes

ThyristorsSCRTRIAC

## Bi-directional switching

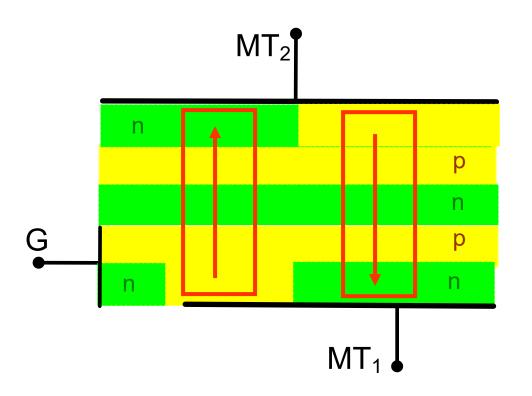


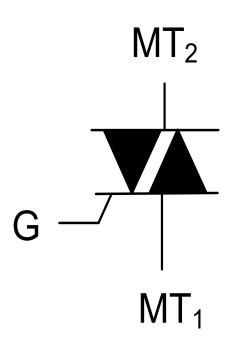
Use two cross-coupled SCRs

#### Limitations

Size and cost overhead with this solution Inconvenient triggering since  $G_1$  and  $G_2$  WRT different terminals

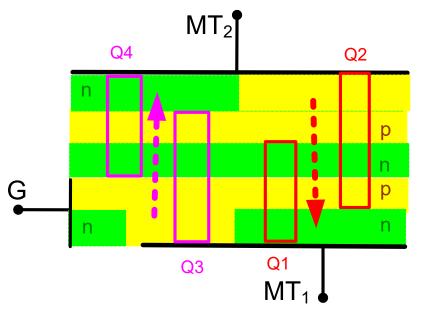
## Bi-directional switching with the Triac

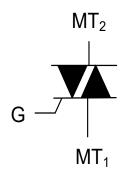




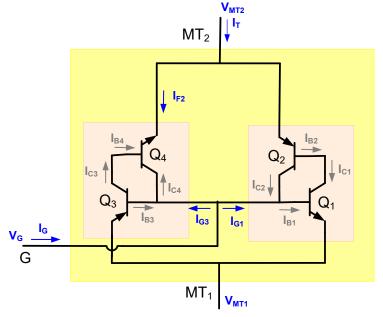
- Has two cross-coupled SCRs!
- Manufactured by diffusions
- Single Gate Control

### The Triac





Can define two cross-coupled transistor pairs in each side



Model for Quadrants 1 and 4 (n-diffusion for gate not shown)

As for SCR, both circuits have regenerative feedback

Can turn ON in either direction with either positive or negative current

Defines 4 quadrants (in V<sub>MT21</sub>-V<sub>G-MT1</sub> plane) for operation

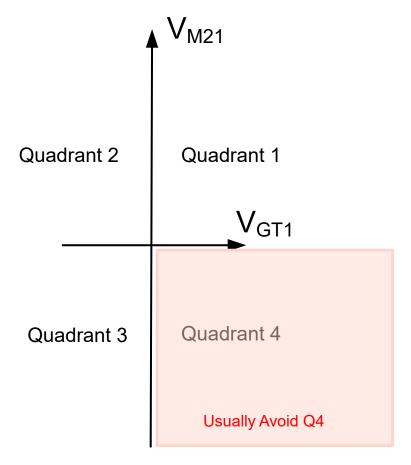
$V_{MT2}>V_{MT1}$	$V_{G-MT1}>0$	Quadrant 1
$V_{MT2}>V_{MT1}$	$V_{G-MT1}$ <0	Quadrant 2
$V_{MT2} < V_{MT1}$	$V_{G-MT1}$ <0	Quadrant 3
$V_{MT2} < V_{MT1}$	V <sub>G-MT1</sub> >0	Quadrant 4

Usually use only one V<sub>G</sub>:V<sub>MT</sub> for control

Different voltage, duration strategies exist for triggering

Can't have single V<sub>G</sub>:V<sub>MT</sub> control with two SCRs

## The Triac



 $\mathsf{MT}_2$ 

 $MT_1$ 

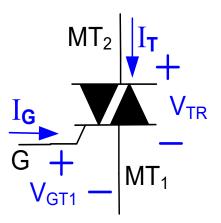
Defines 4 quadrants (in  $V_{MT21}$ - $V_{G-MT1}$  plane) for operation

$V_{MT2}>V_{MT1}$	$V_{G-MT1}>0$	Quadrant 1
$V_{MT2}>V_{MT1}$	$V_{G-MT1}$ <0	Quadrant 2
$V_{MT2} < V_{MT1}$	$V_{G-MT1}$ <0	Quadrant 3
$V_{MT2} < V_{MT1}$	$V_{G-MT1}>0$	Quadrant 4

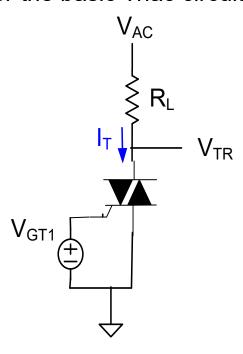
#### The ideal Triac

# $I_G=0$ $-V_{BGF}$ $I_G=I_{G1}<0$ or $-V_{\text{BGF}}$

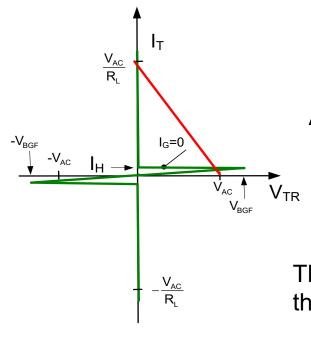
## The Triac



#### Consider the basic Triac circuit



## Assume ideal Triac with I<sub>G</sub>=0 The Basic Triac Circuit

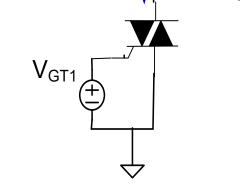


Load Line:  $V_{AC} = I_{T}R_{L} + V_{TR}$ 

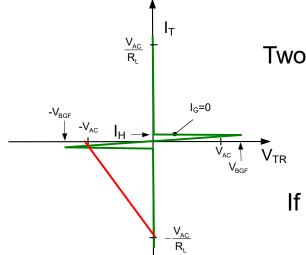
Analysis:

$$V_{AC} = I_{T}R_{L} + V_{TR}$$

$$I_{T} = f_{A}(V_{TR}, V_{GT1})$$



The solution of these two equations is at the intersection of the load line and the device characteristics

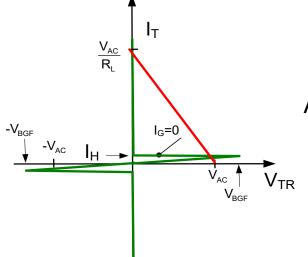


Two stable operating points for both positive and negative  $V_{AC}$ 

If V<sub>AC</sub> is a sinusoidal signal, will stay OFF Why?

Assume ideal Triac with  $I_G = 0$ 

## The Basic Triac Circuit

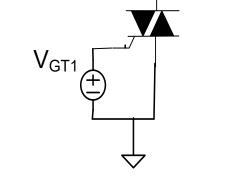


Load Line:  $V_{AC} = I_{T}R_{L} + V_{TR}$ 

Analysis:

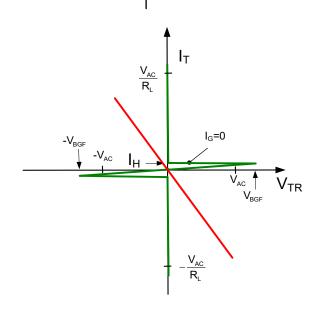
$$V_{AC} = I_{T}R_{L} + V_{TR}$$

$$I_{T} = f_{A}(V_{TR}, V_{GT1})$$



If V<sub>AC</sub> is a sinusoidal signal, will stay OFF

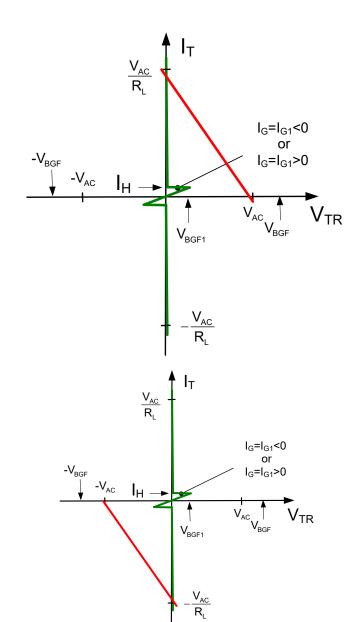
Why?



Because when it goes through 0 there is only one solution and that corresponds to the OFF state

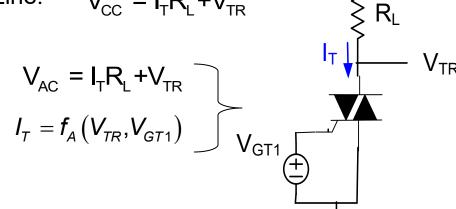
Assume ideal Triac with large I<sub>G</sub>





Load Line:  $V_{CC} = I_T R_L + V_{TR}$ 

Analysis:

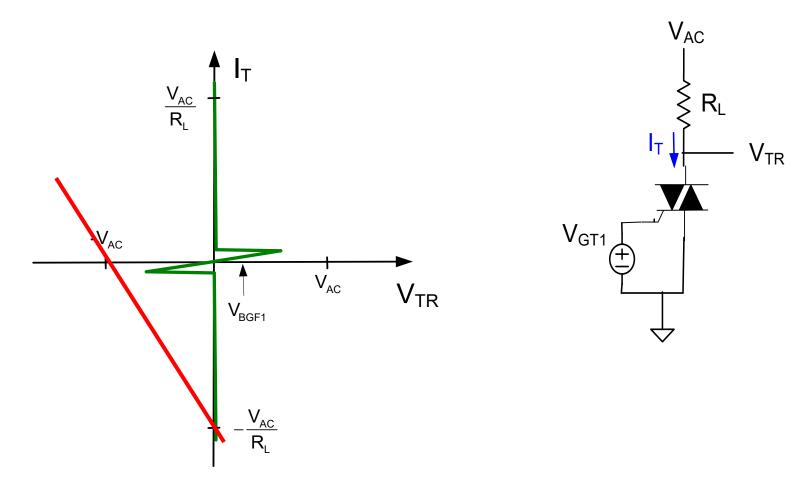


Single solution for both positive and negative  $V_{AC}$ 

If  $V_{AC}$  is a sinusoidal signal will stay ON

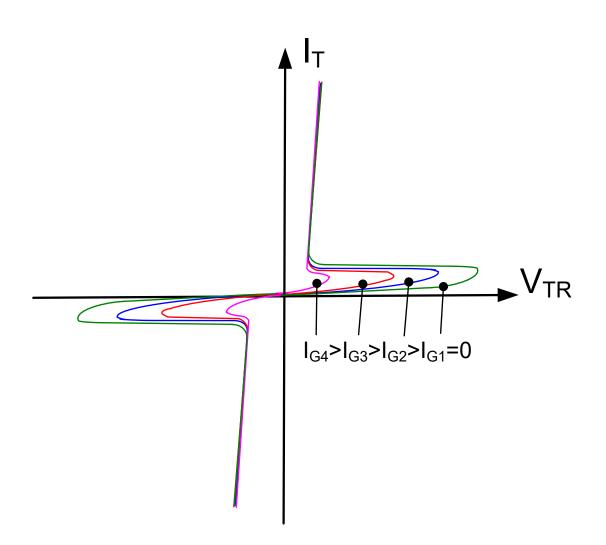
(except for small time when  $I_T$ =0 but then ON and OFF state of Triac do not alter current in circuit)

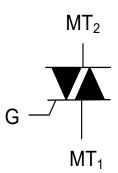
### The Basic Triac Circuit



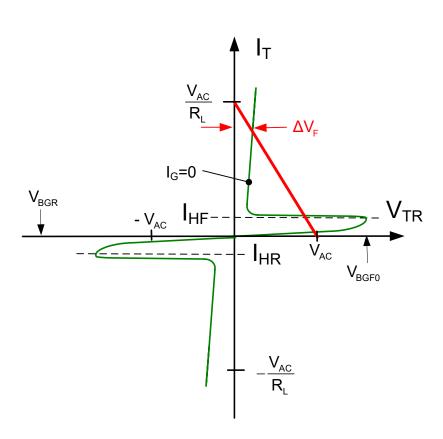
Duty cycle can vary from near 0% to 100% depending on  $I_G$  (or  $V_{GT1}$ )

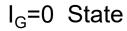
## The Actual Triac

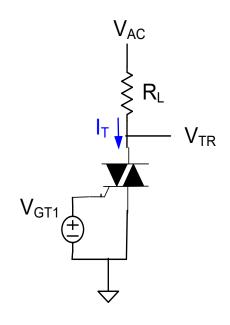




## The Actual Triac in Basic Circuit

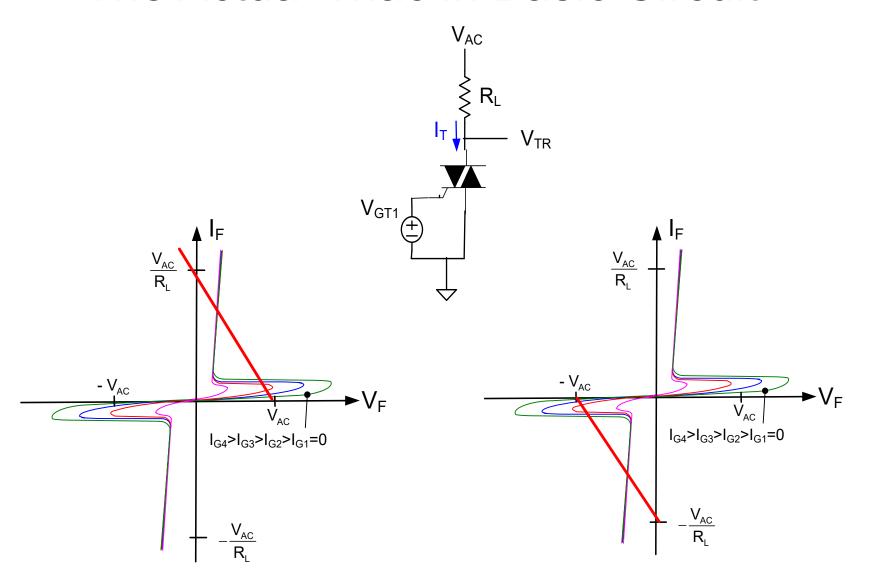






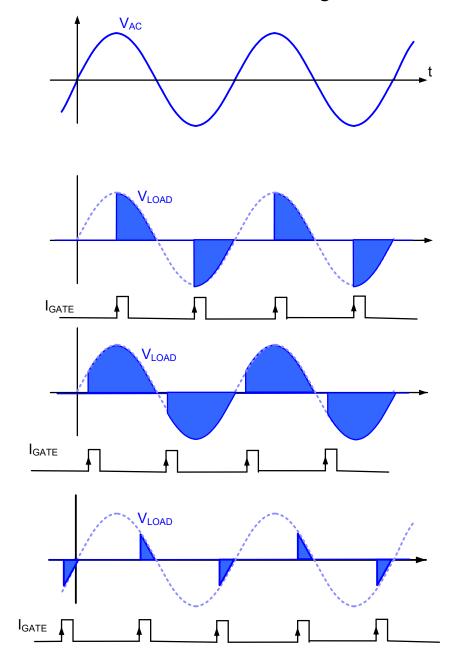
Two stable operating points (as long as V<sub>AC</sub> not near 0)

## The Actual Triac in Basic Circuit



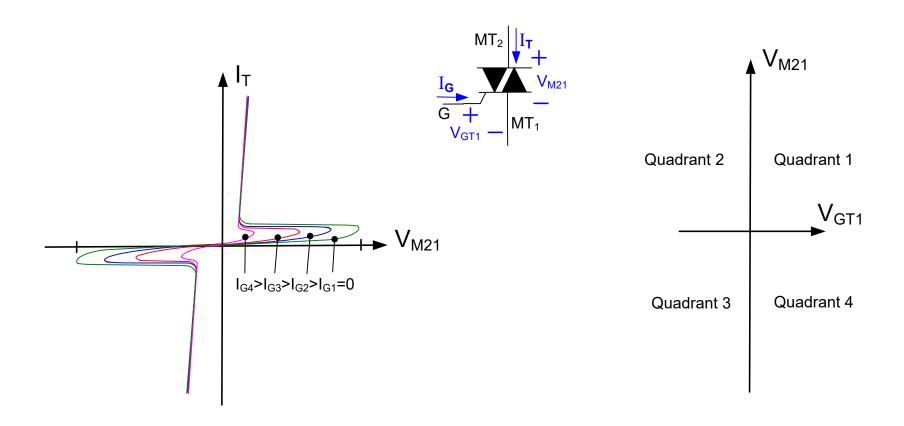
Can turn on for either positive or negative  $V_{AC}$  with single gate signal

#### Phase controlled bidirectional switching with Triacs



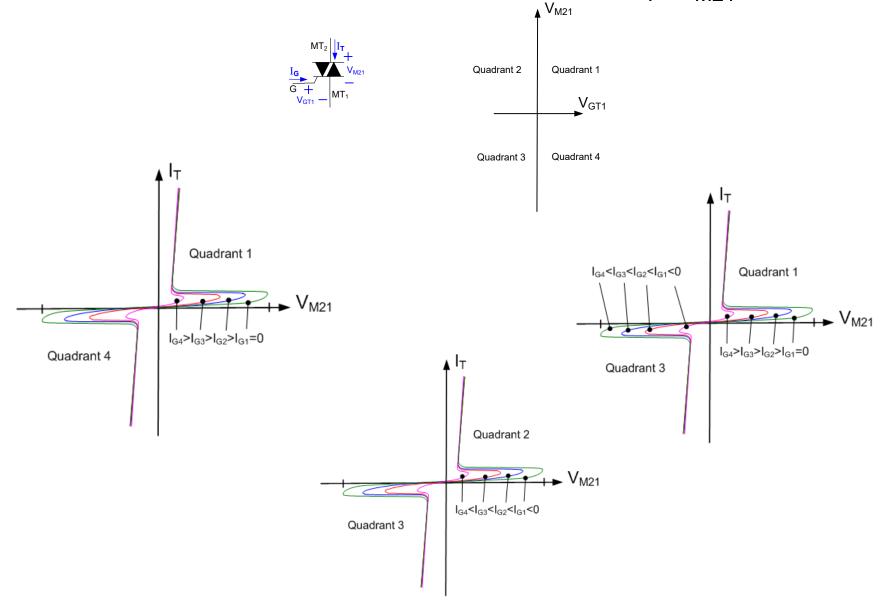
## Quadrants of Operation Defined in V<sub>M21</sub>-V<sub>GT1</sub> plane

(not in the  $I_T$ - $V_{M21}$  plane)

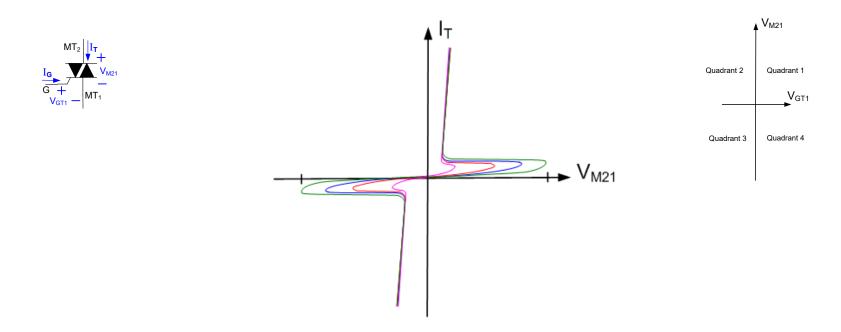


But for any specific circuit, can map quadrants from the  $V_{M21}$ - $V_{GT1}$  plane to  $I_T$ - $V_{M21}$  plane

#### Identification of Quadrants of Operation in I<sub>T</sub>-V<sub>M21</sub> plane



#### Identification of Quadrants of Operation in I<sub>T</sub>-V<sub>M21</sub> plane

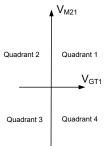


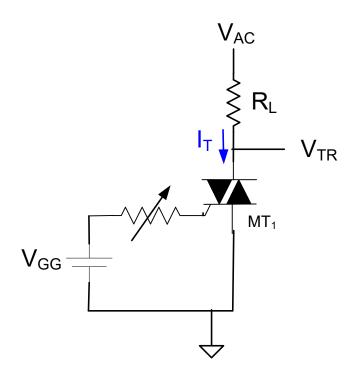
Curves may not be symmetric between  $Q_1$  and  $Q_3$  in the  $I_T$ - $V_{M21}$  plane

Turn on current may be large and variable in  $Q_4$  (of the  $V_{M21}$ - $V_{GT1}$ )

Generally avoid operation in  $Q_4$  (of the  $V_{M21}$ - $V_{GT1}$  plane)

Most common to operate in Q2-Q3 quadrants or Q1-Q3 quadrants (of the V<sub>M21</sub>-V<sub>GT1</sub> plane)

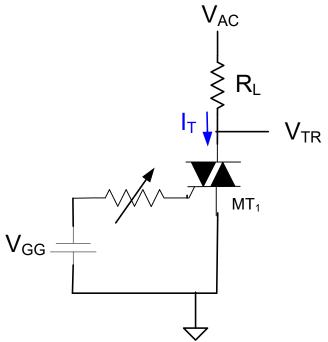




(V<sub>GG</sub> often from logic/control circuit)

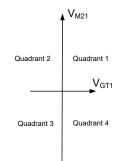
Quad 1: Quad 4

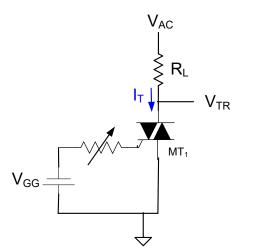
(not attractive because of Quad 4)



(V<sub>GG</sub> often from logic/control circuit)

Quad 2: Quad 3



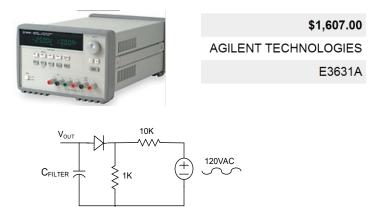


Quad 2: Quad 3

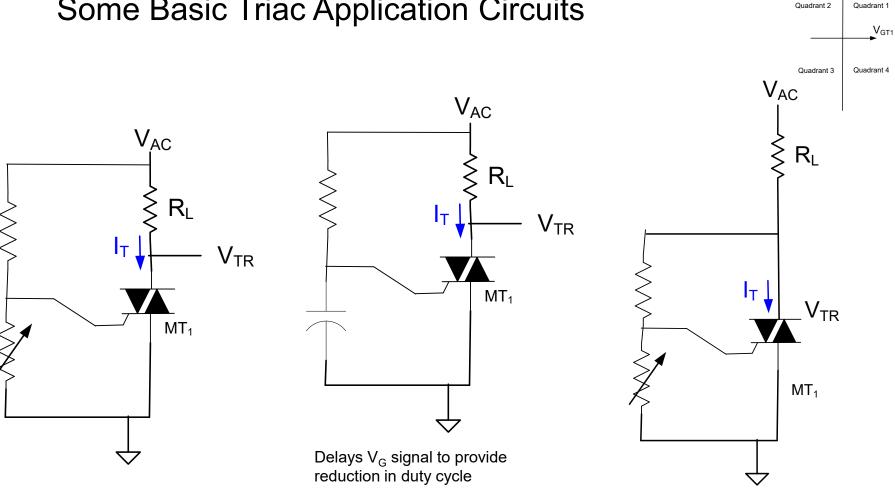
#### Limitations?

If V<sub>AC</sub> is the standard 120VAC line voltage, where do we get the dc

power supply?



Direct digital control of trigger voltage/current with dedicated IC

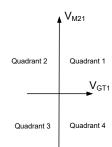


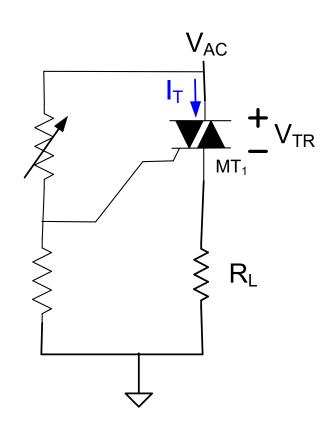
Quad 1: Quad 3

Quad 1: Quad 3

Quad 1: Quad 3

 $_{A}$   $V_{M21}$ 





Quad 1/ Quad 2: Quad 4/Quad 3

 $R_L$  $I_{T}$ Logic and/or Interface Circuit  $MT_1$ (with negative logic levels)

 $V_{AC}$ 

Real popular

Not real popular

# **Thyristor Types**

Some of the more major types:

- SCR
- Triac
- Bidirectional Phase-controlled thyristors (BCT)
- LASCR (Light activated SCR)
- Gate Turn-off thyristors (GTO)
- FET-controlled thyristors(FET-CTH)
- MOS Turn-off thyristors (MTO)
- MOS-controlled thyristors (MCT)

# **Thyristor Applications**

Thyristors are available for working at very low current levels in electronic circuits to moderate current levels such is in incandescent light dimmers to very high current levels

I<sub>TRIAC</sub> from under 1mA to 10000A

Applications most prevalent for moderate to high current thyristors



SCR, rated about 100 amperes, 1200 volts, 1/2 inch stud, photographed by C J Cowie. Uploaded on 4 April 2006.



#### PT40QPx45

#### **Pulse Power Thyristor Switch**

Preliminary Information

DS5267-1.4 April 2000

Replaces November 1999 version, DS5267-1.1

#### **APPLICATIONS**

- Pulse Power
- Crowbars
- Ignitron Replacement

 $\begin{array}{ccc} \text{KEY PARAMETERS} \\ \text{V}_{\text{DRM}} & 4500\text{V} \\ \text{I}_{\text{T(AV)}} & 760\text{A} \\ \text{I}_{\text{TSM}} & 13000\text{A} \\ \text{dI/dt} & 5000\text{A/}\mu\text{s} \end{array}$ 

I<sub>TSM</sub> is the non-repetitive surge peak current

Important parameter to consider when switching inductive loads (motors)

#### From ABB Web Site

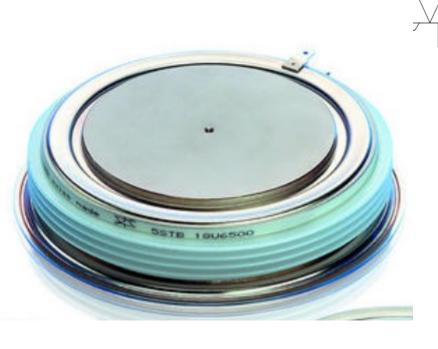
 $V_{RM}$  = 6500 V  $I_{T(AV)M}$  = 1405 A  $I_{T(RMS)}$  = 2205 A  $I_{TSM}$  = 22×10<sup>3</sup> A

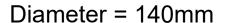
 $I_{TSM} = 22 \times 10^3 \text{ A}$   $V_{T0} = 1.2 \text{ V}$ 

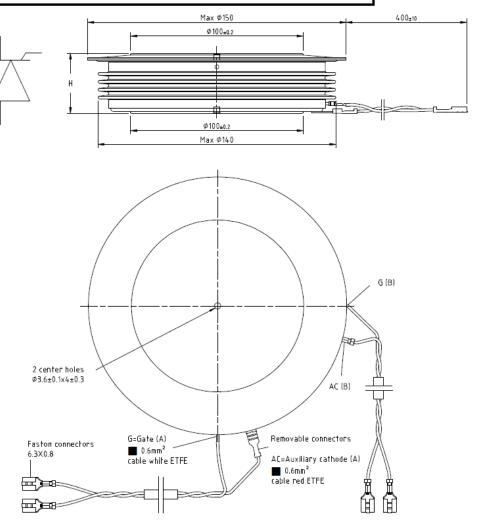
 $r_T = 0.6 \,\mathrm{m}\Omega$ 

#### **Bi-Directional Control Thyristor**

5STB 13N6500







## Thanks to Prof. Ajjarapu for providing the following slides: THE BIDIRECTIONAL CONTROL THYRISTOR (BCT)

by

Kenneth M. Thomas, Björn Backlund, Orhan Toker ABB Semiconductors AG, CH5600 Lenzburg, Switzerland

Björn Thorvaldsson ABB Power Systems AB, S-721 64 Västerås, Sweden

#### **ABSTRACT**

The Bidirectional Control Thyristor (BCT) is a new concept for high power thyristors integrated on a single silicon wafer with separate gate contacts. This unique design, based on free-floating silicon technology, successfully overcomes the traditional problems of interference experienced by bidirectional thyristors during dynamic operation which previously prevented the use of such devices. Such components are suitable for applications at high voltages like a normal thyristor but where triacs can no longer be used.

# High Current, High Voltage Solid State Discharge Switches for Electromagnetic Launch Applications

A. Welleman, R. Leutwyler, J. Waldmeyer ABB Switzerland Ltd, Semiconductors - CH-5600 Lenzburg

Abstract—This presentation is about the work done on design, built-up, production and test of ready-to-use solid state switch assemblies using Thyristor- or IGCT technology. The presented thyristor switch assemblies, using 120 mm wafer size, are made to switch 3MJ stored energy into a load. The maximum charge voltage of the assembly is 12 kVdc, current capability more than 260kA@tp=3.3ms and a pulse repetition rate of up to 6 shots per minute with convection air cooling. New very large thyristors with 150 mm vafer diameter will be available from fall 2008. As second a 70 kA/21kVdc switch using IGCT technology will be presented. The switch is designed for fast discharge in the microsecond range and has a very high di/dt capability. Because for

adapted standard products which can fulfill the requirements for pulsed applications. Beside the semiconductor devices, ABB is also in the position to supply complete custom made ready-to-use solid state switch assemblies including clamping, triggering, cooling and with application oriented testing. The presentation describes both, the loose semiconductor components as well as some custom made solid state switches for single pulse or low repetition rate pulsing.

II. DEVICE TECHNOLOGY

2008 Paper

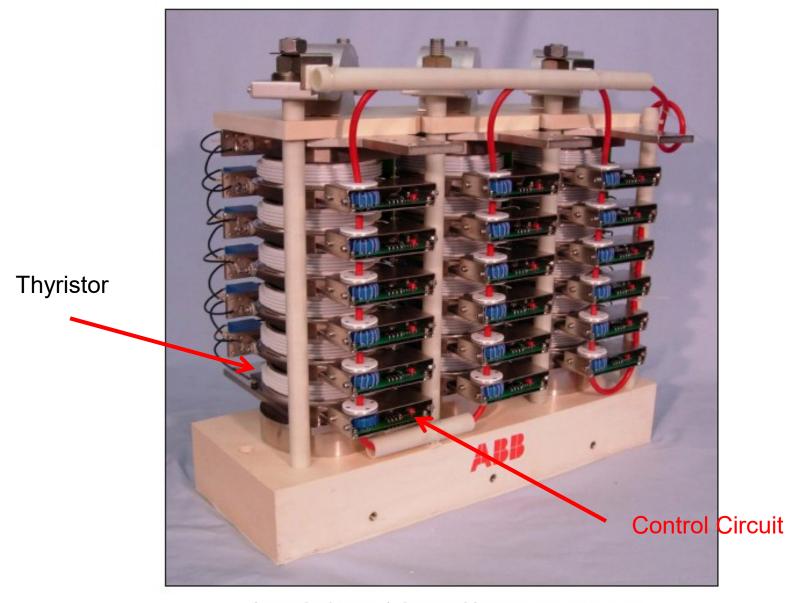
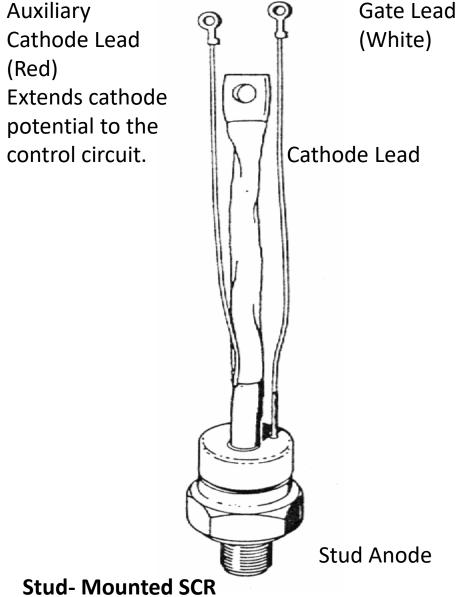
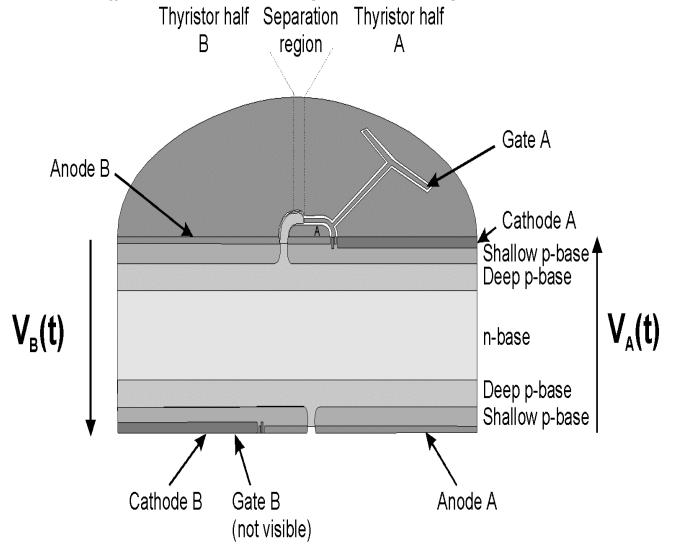


Fig.3: Thyristor Switch Assembly A-STP 5742U-18-CC



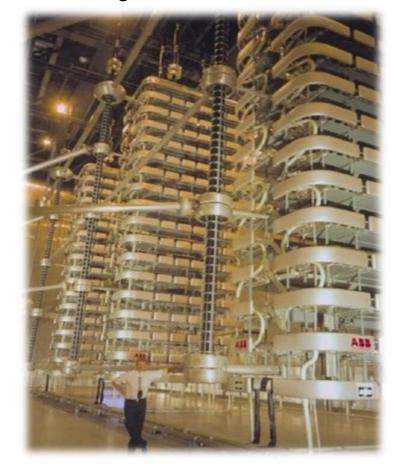
110 Amp RMS Rating



Cross-section of a BCT wafer showing the antiparallel arrangement of the A and B component thyristors. The arrows indicate the convention of forward blocking for A and B.

Thanks to Prof. Ajjarapu for providing the following slides:





Thyristor Valve - 12 Pulse Converter (6.5Kv, 1568 Amp, Water cooled)

# **Thyristor Observations**

Many different structures used to build thyristors

Range from low power devices to extremely high power devices

Often single-wafer solutions for high power applications

Usually formed by diffusions

Widely used throughout society but little visibility

Applications somewhat restricted

## **Thyristors**

The good

SCRs Triacs

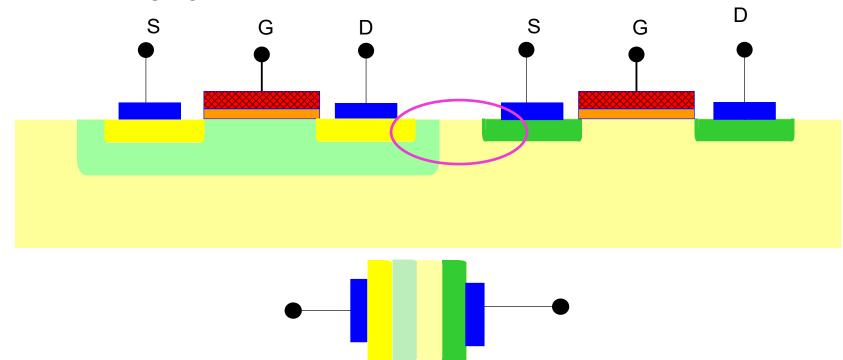
The bad

Parasitic Device that can destroy integrated circuits

## The Thyristor

A bipolar device in CMOS Processes

Consider a Bulk-CMOS Process



If this parasitic SCR turns on, either circuit will latch up or destroy itself Guard rings must be included to prevent latchup

Design rules generally include provisions for guard rings



Stay Safe and Stay Healthy!

## End of Lecture 30